

NASA MFC Piezocomposites: A Development History

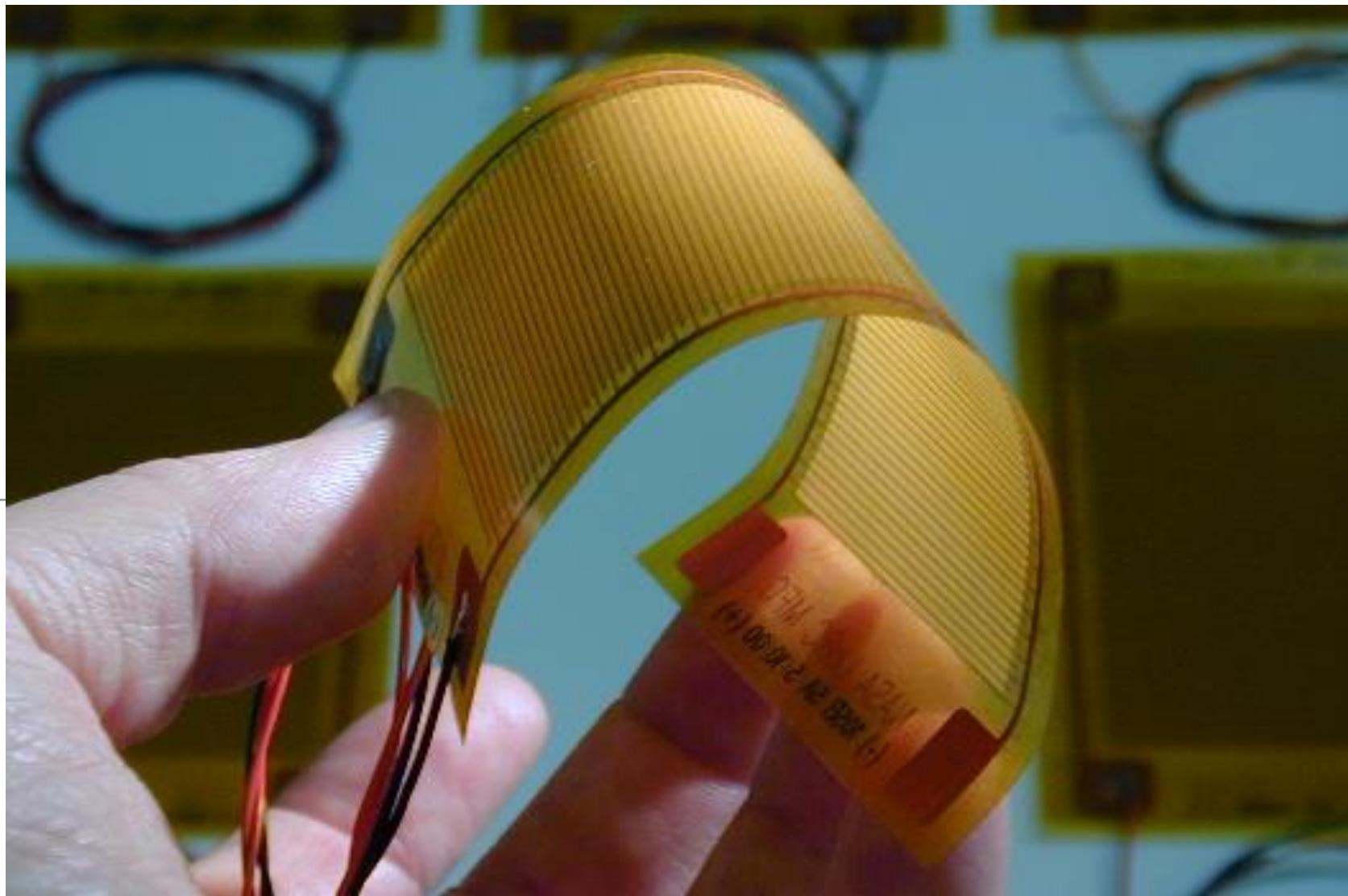
W. Keats Wilkie

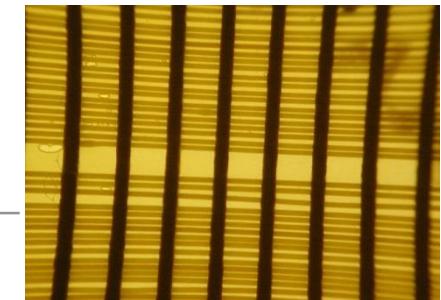
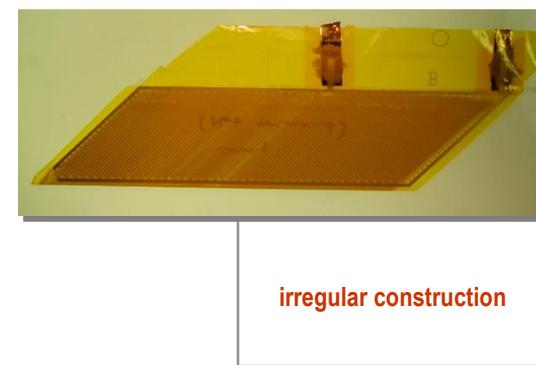
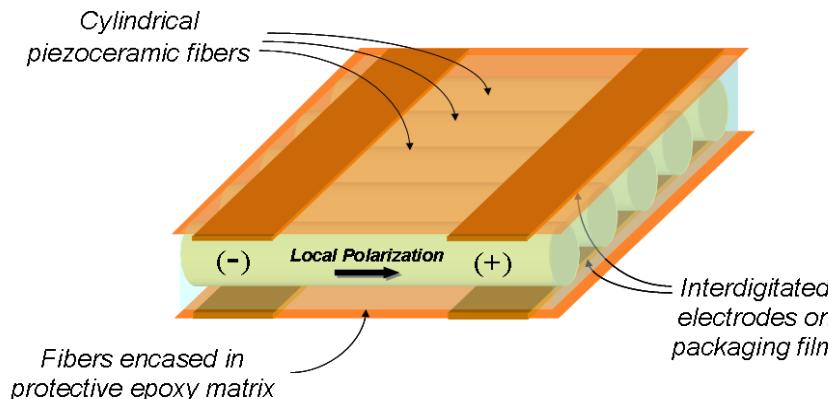
Senior Member Technical Staff

Mechanical Systems Engineering Research Division

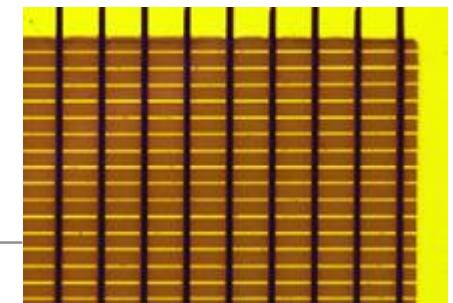
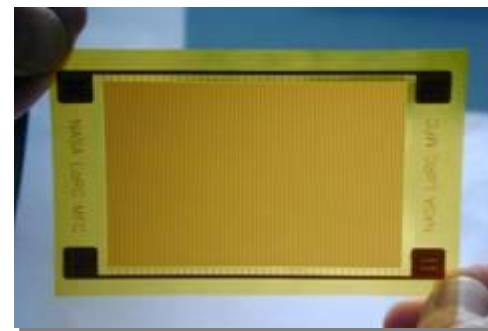
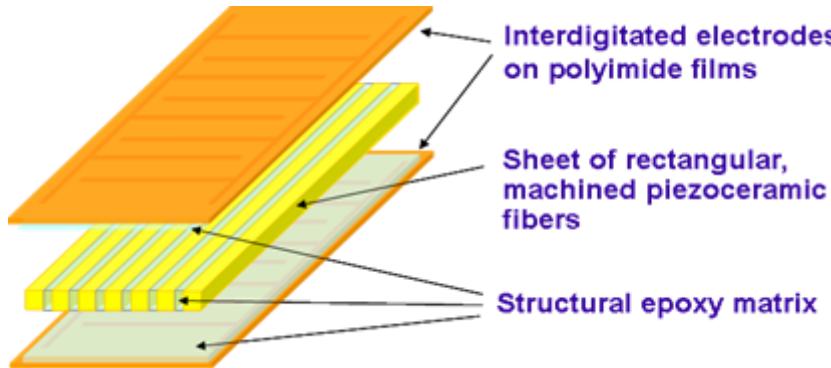
NASA Jet Propulsion Laboratory

California Institute of Technology



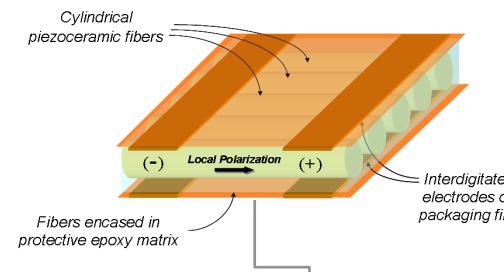


1st generation device: AFC (MIT, 1993-2000)

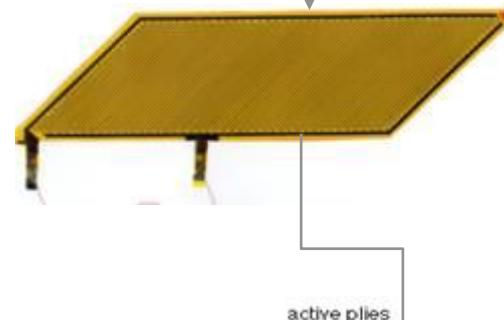


Advanced piezocomposite: MFC (NASA, ARL, 1997-2003)

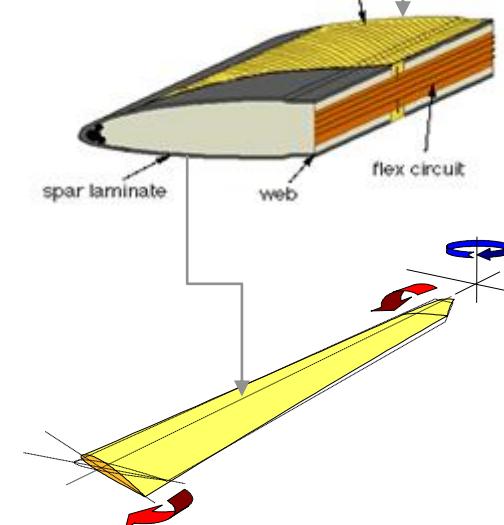
1. Piezoelectric Composite Actuator



2. Active Fiber Composite Plies

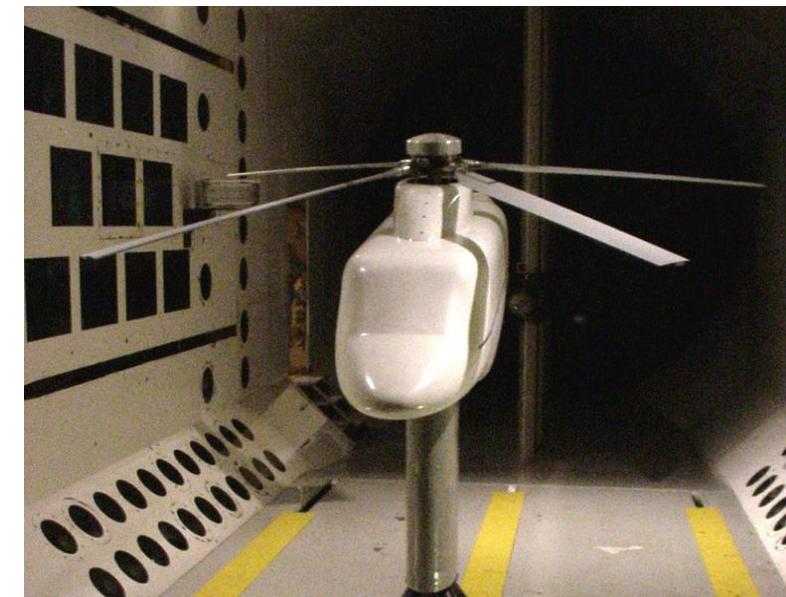


3. Active Composite Structure

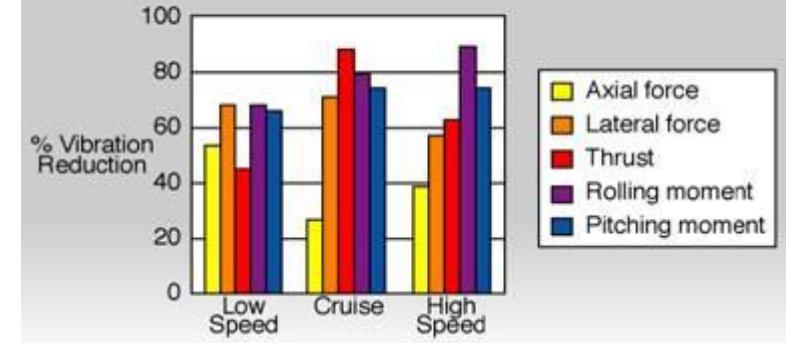


4. Active Twist Control

4. Active Twist Rotor In Wind Tunnel

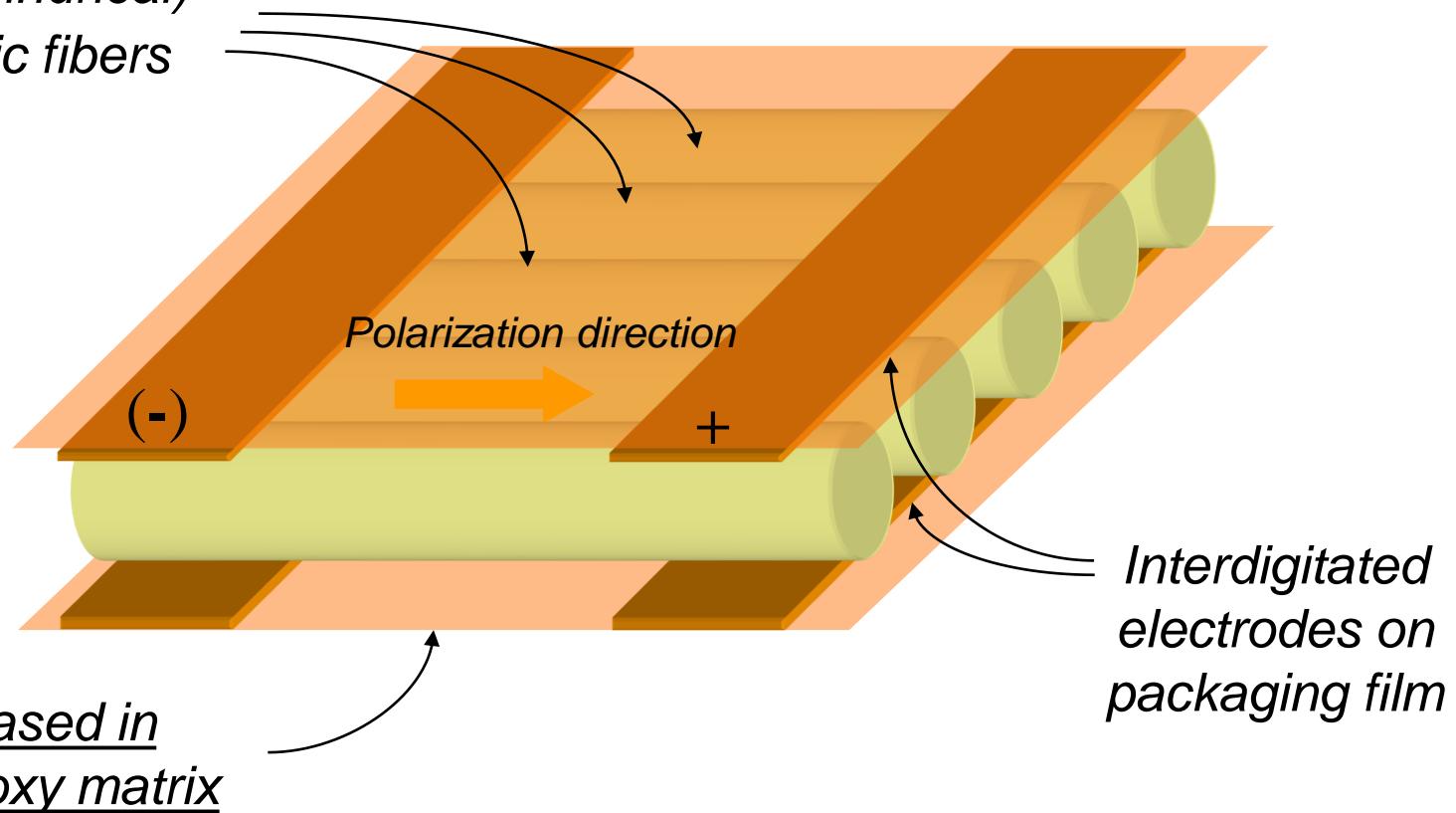


Measured Closed-Loop Vibration reduction of fixed-System Loads



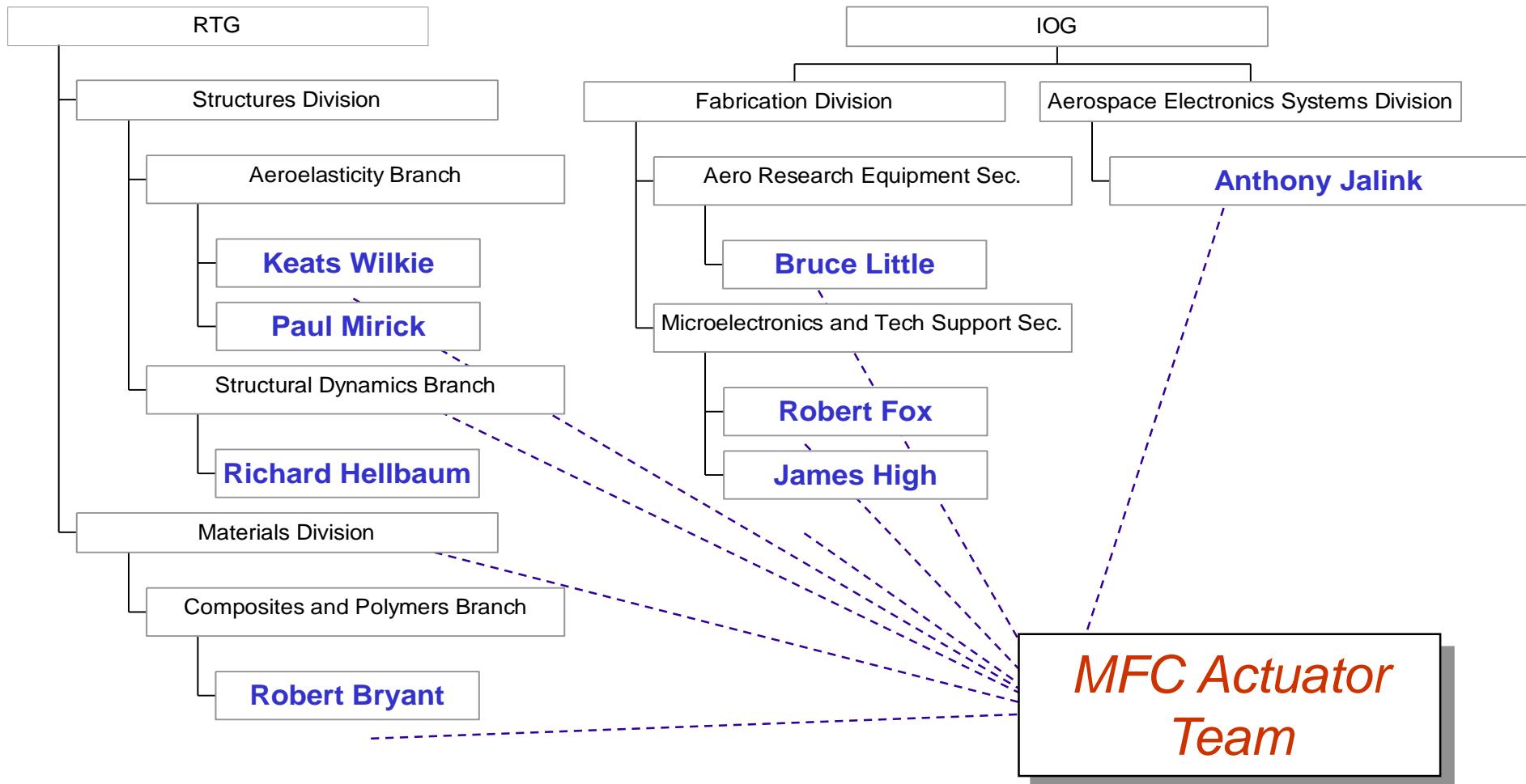
(MIT, 1995)

*Extruded (cylindrical)
piezoceramic fibers*

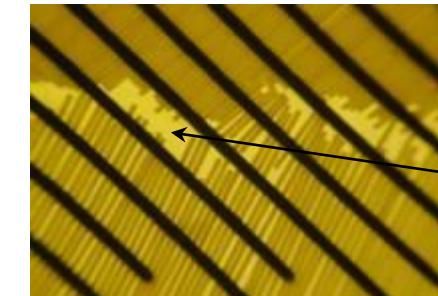


Fibers encased in
protective epoxy matrix

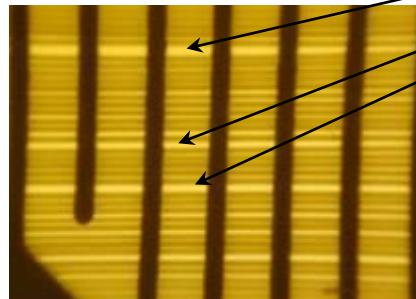
*Interdigitated
electrodes on
packaging film*



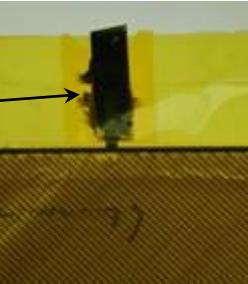
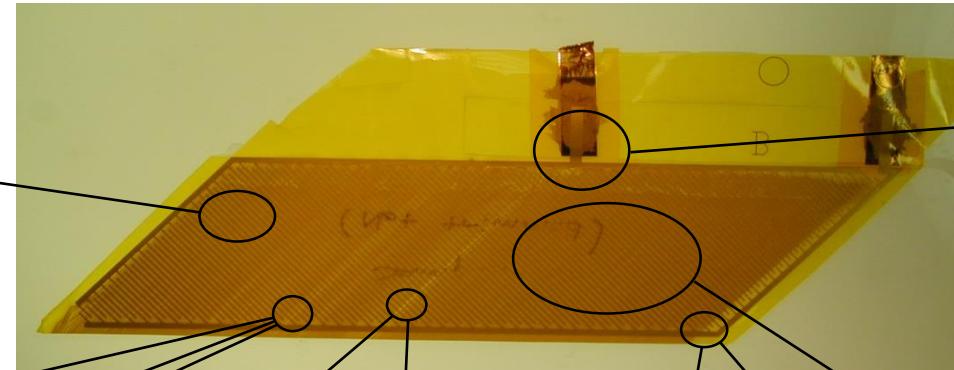
NASA Langley Research Center (LaRC), ca. December 1997



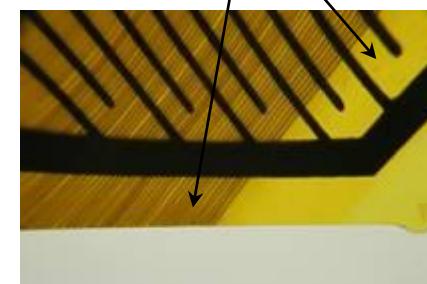
Fiber Breakage



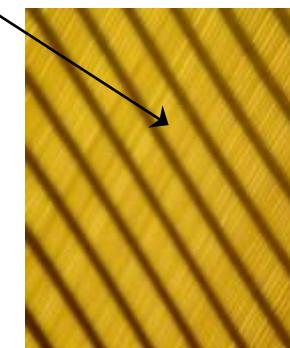
Fiber Distribution



Electrical Connects



Non-uniform
Perimeter

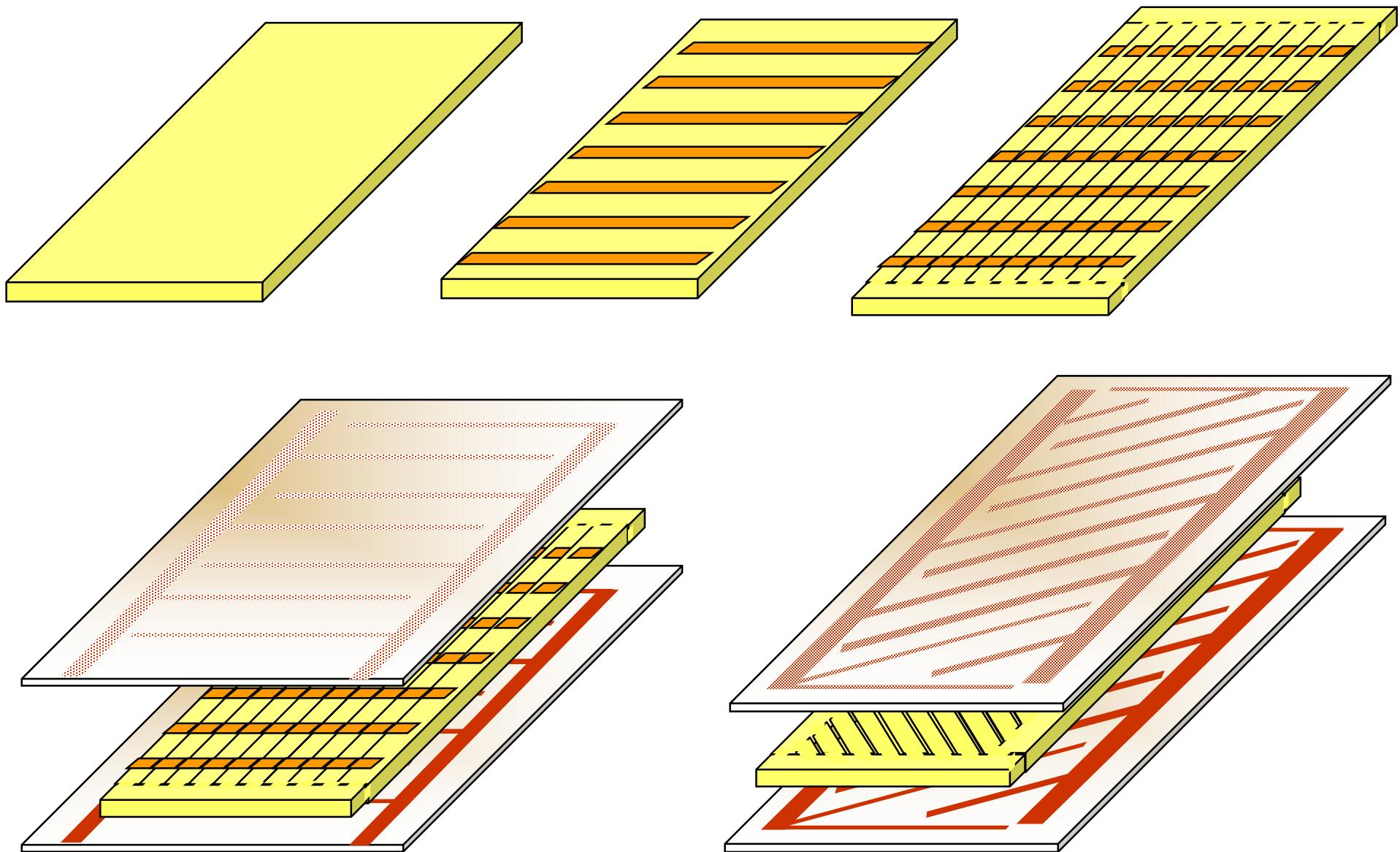


Uniform
Areas

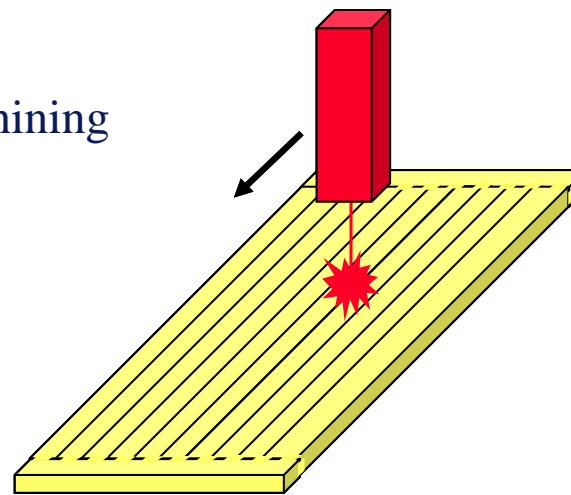


Inclusions

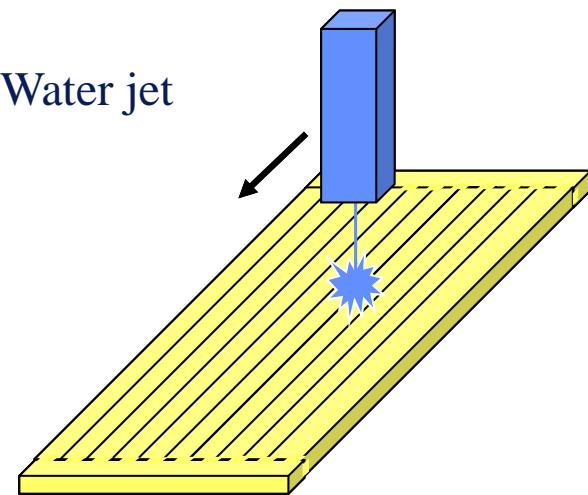
Leads to a Wide Variance in Electro-Mechanical Properties



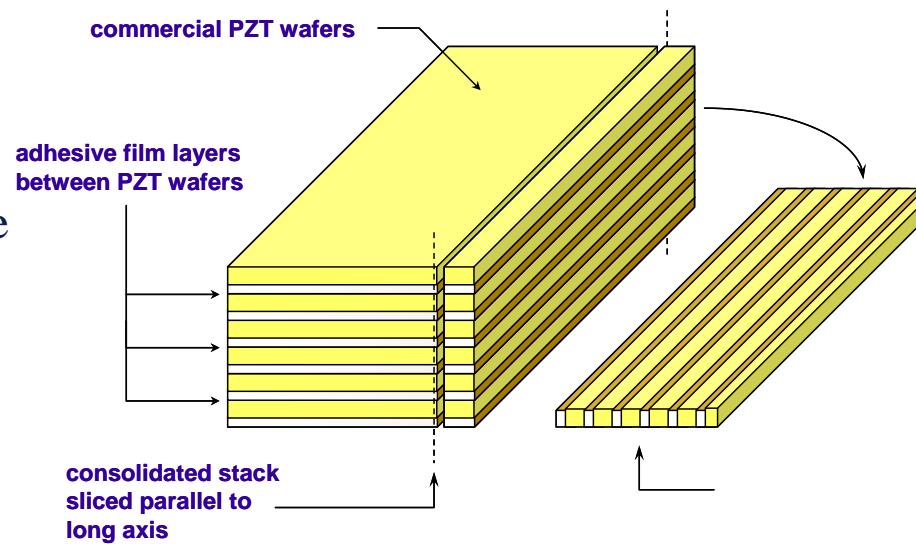
1. Laser machining

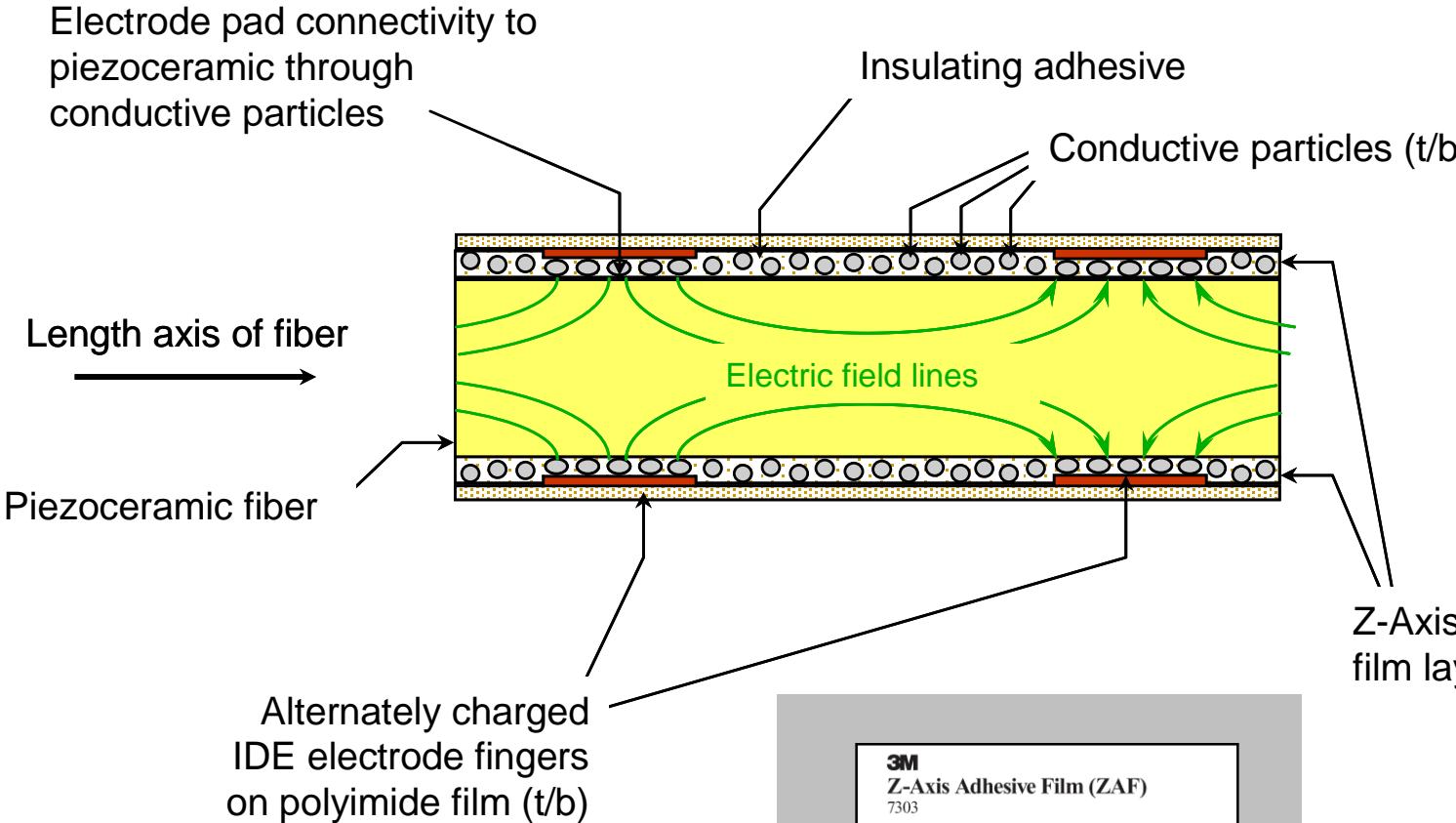


2. Water jet

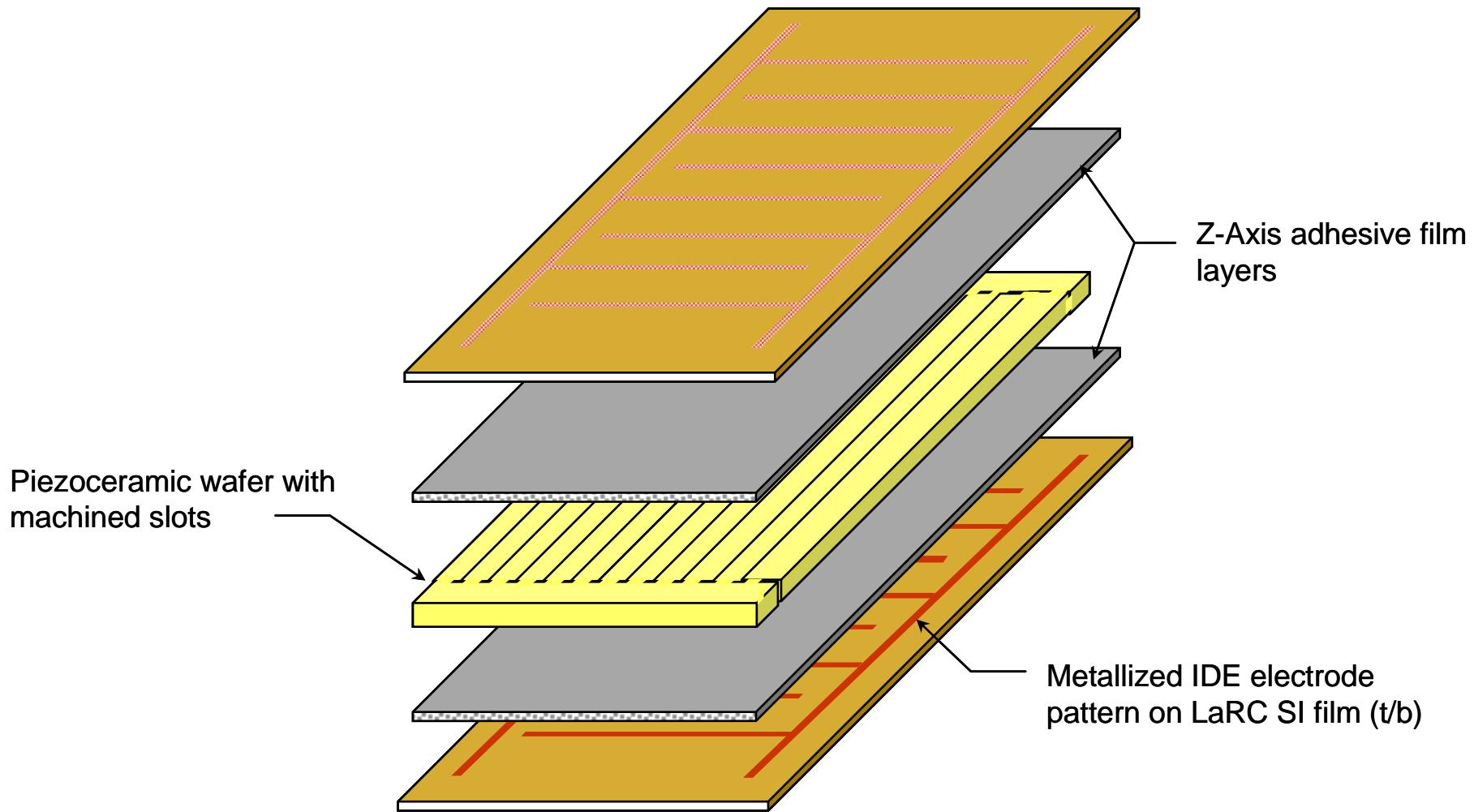


3. Stack and slice





Ref: <http://www.3m.com>

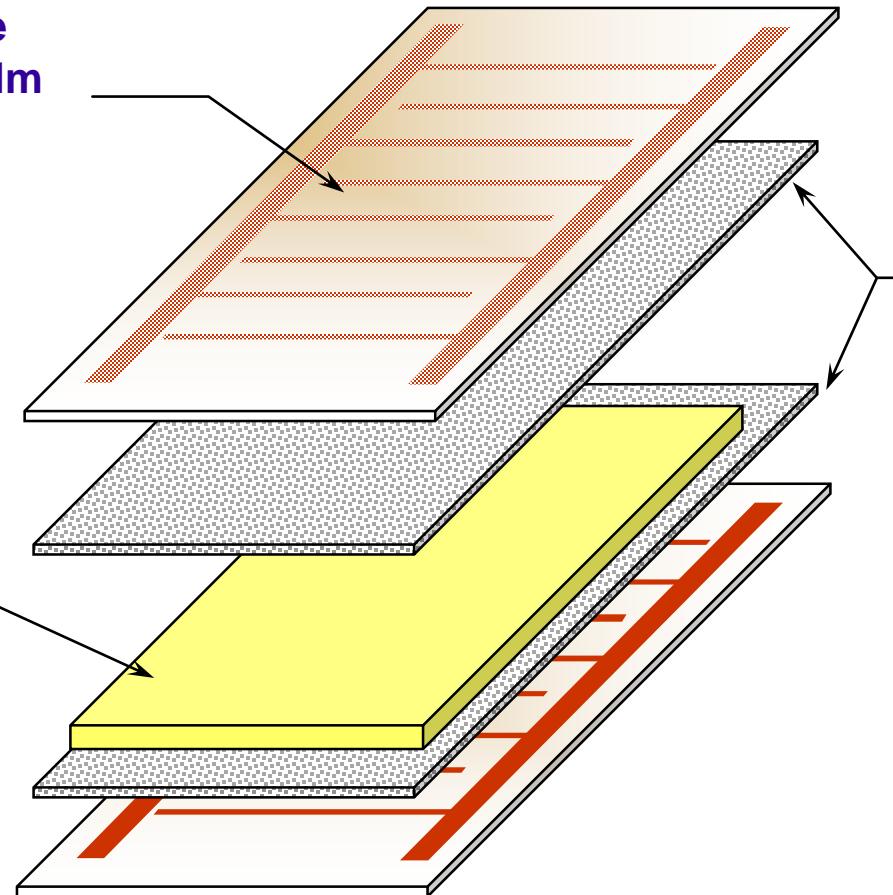


Interdigitated electrode pattern on polyimide film (t/b)

Permits *in-plane poling* and actuation of piezoceramic (d_{11} versus d_{31} advantage)

Monolithic PZT wafer

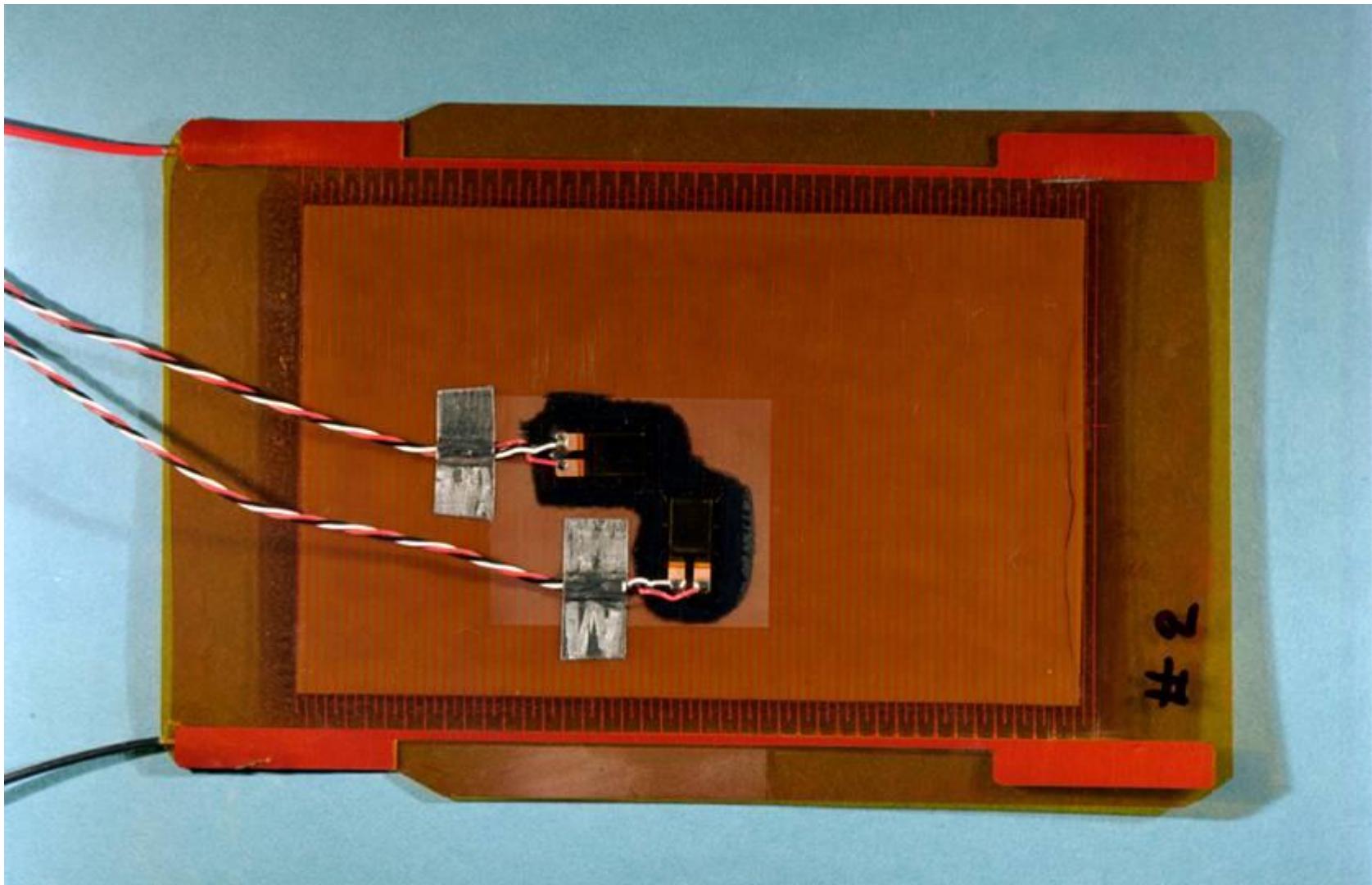
Electrode rails not in direct contact with ceramic. (Eliminates cracking due to nonuniform field near rails.)



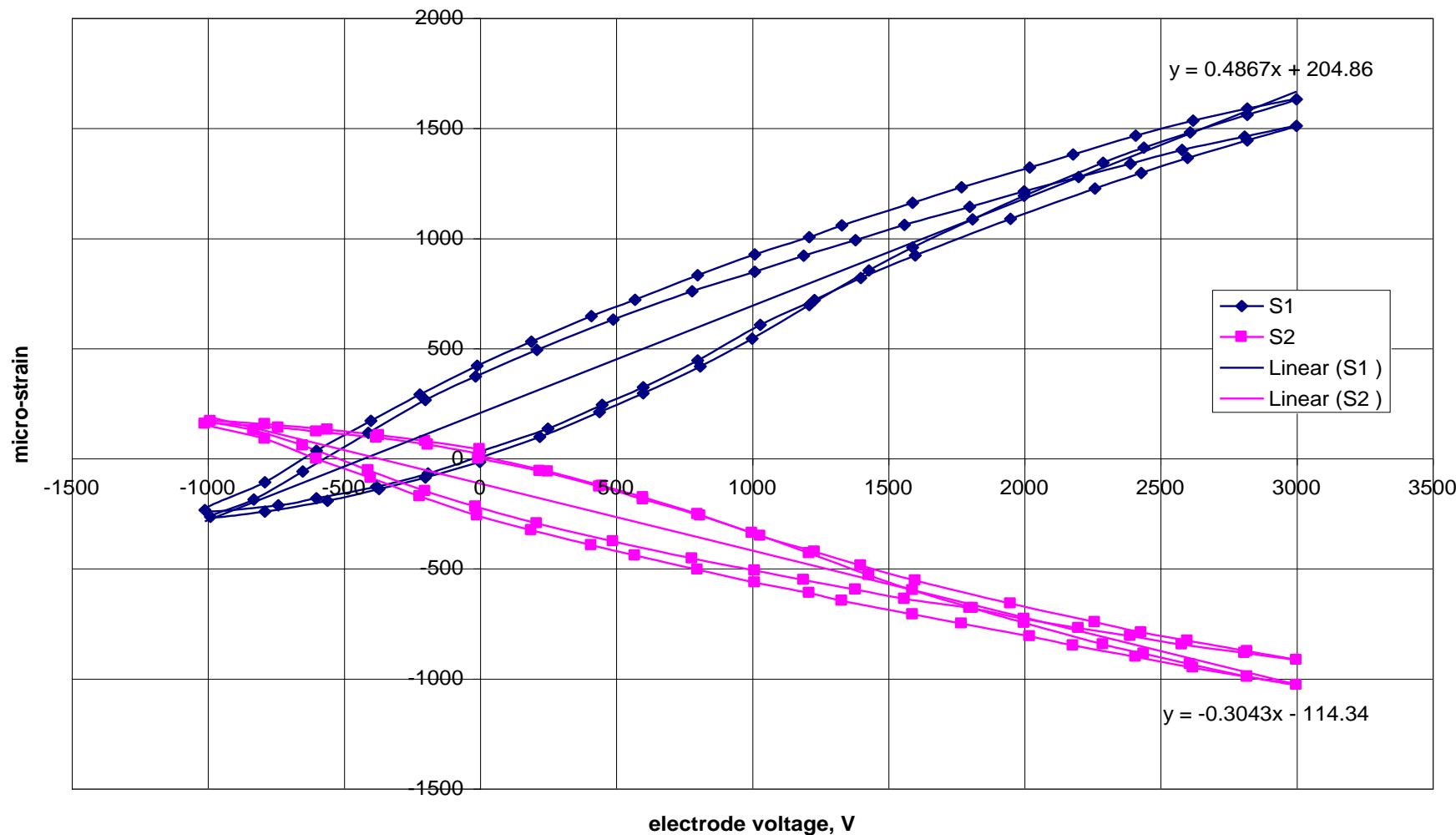
Electrode attachment with either:

- (a) anisotropically conductive adhesive,
- (b) structural epoxy with starved bond-line between electrodes and PZT

Reduces operating voltage by enabling direct electrical contact of electrodes and piezoceramic

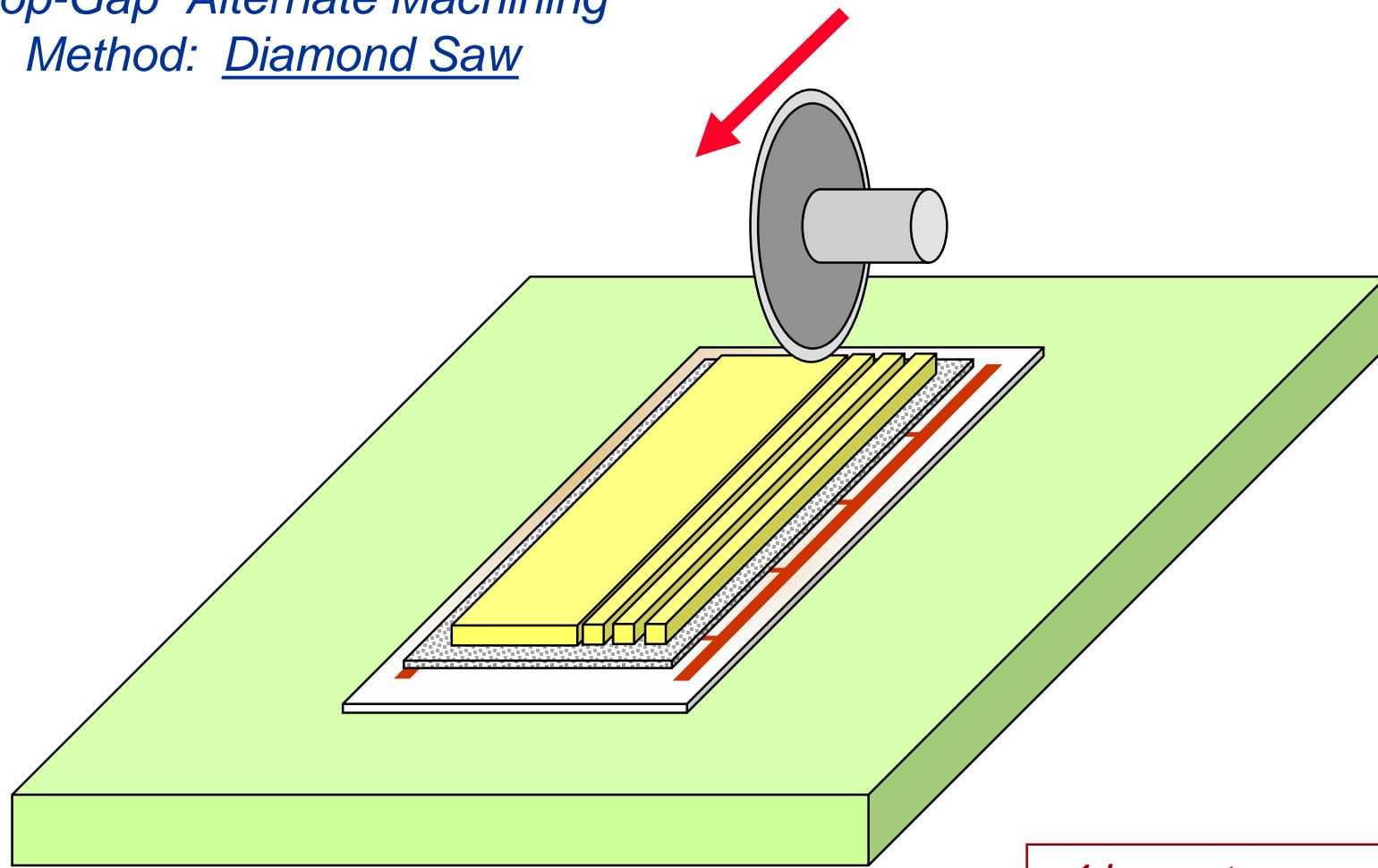


LAFC-0-08a: free-displacement test (rep cycle)



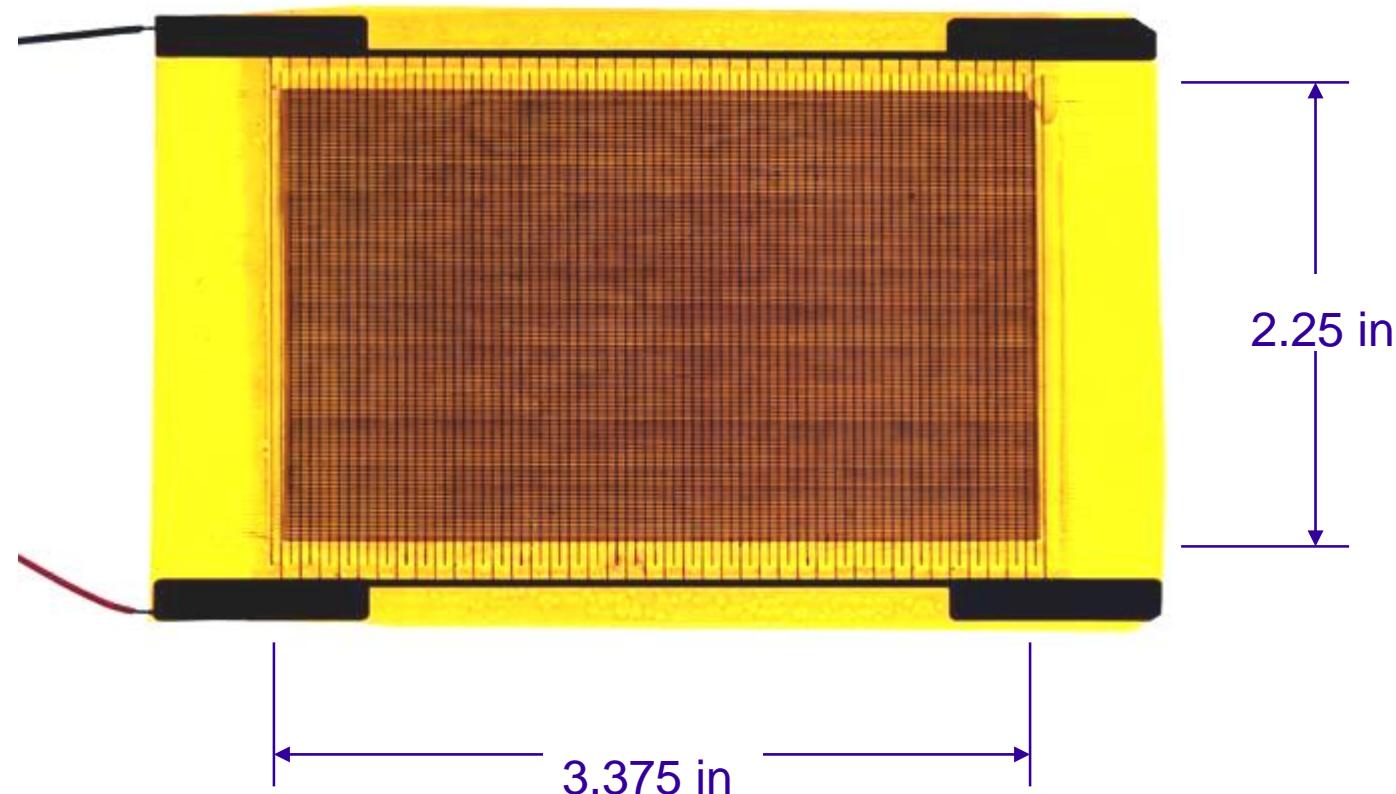
"Stop-Gap" Alternate Machining

Method: Diamond Saw

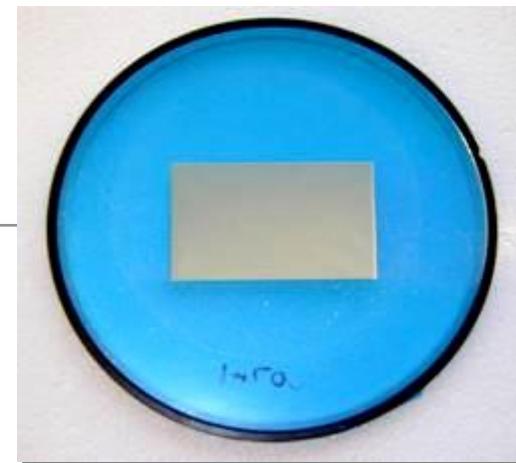


4 hours to complete one
3.375 x 2.25 in wafer!

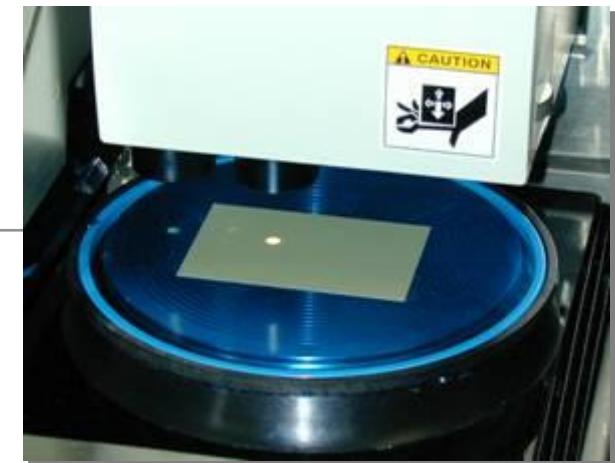
Machined PZT Fiber Prototype: Actuator thickness = 0.011



**Semiconductor wafer
dicing saw**



**1. Ceramic wafer on
grip-tape frame**

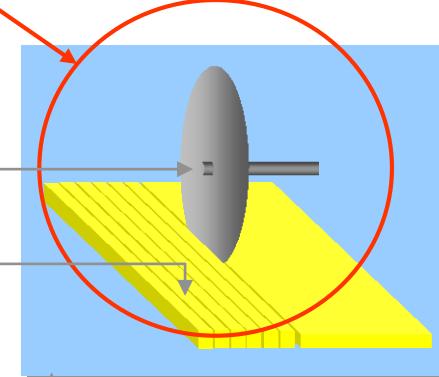


**2. Wafer and grip-tape frame
positioned for dicing**

**Diamond saw blade
(1 - 3 mil thick)**

**Piezoceramic wafer
(5 - 9 mil thick)**

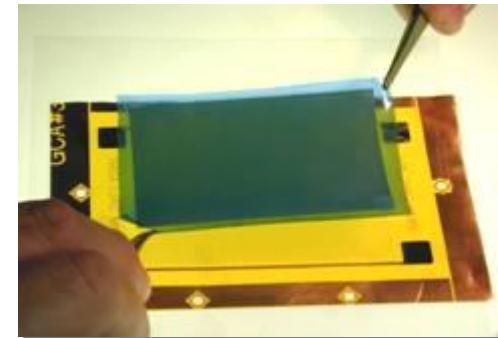
**Polymer grip film
(5 mil thick)**



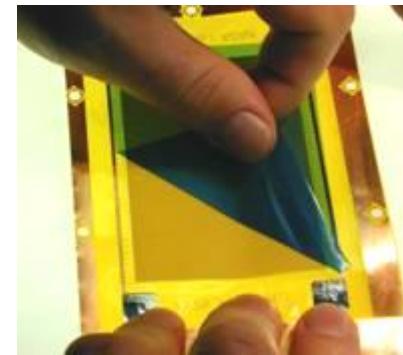
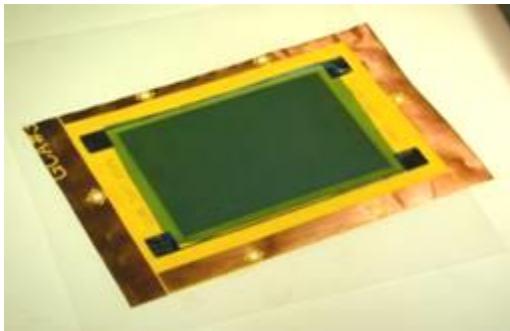
3. Completed piezoceramic fiber sheet



a) Preparation of bottom electrode film with epoxy adhesive.



b) Placement of fiber sheet on electrode film.



c) Fiber sheet and electrode film after heat tacking.



d) Removal of polymer carrier film from transferred piezoceramic fibers.

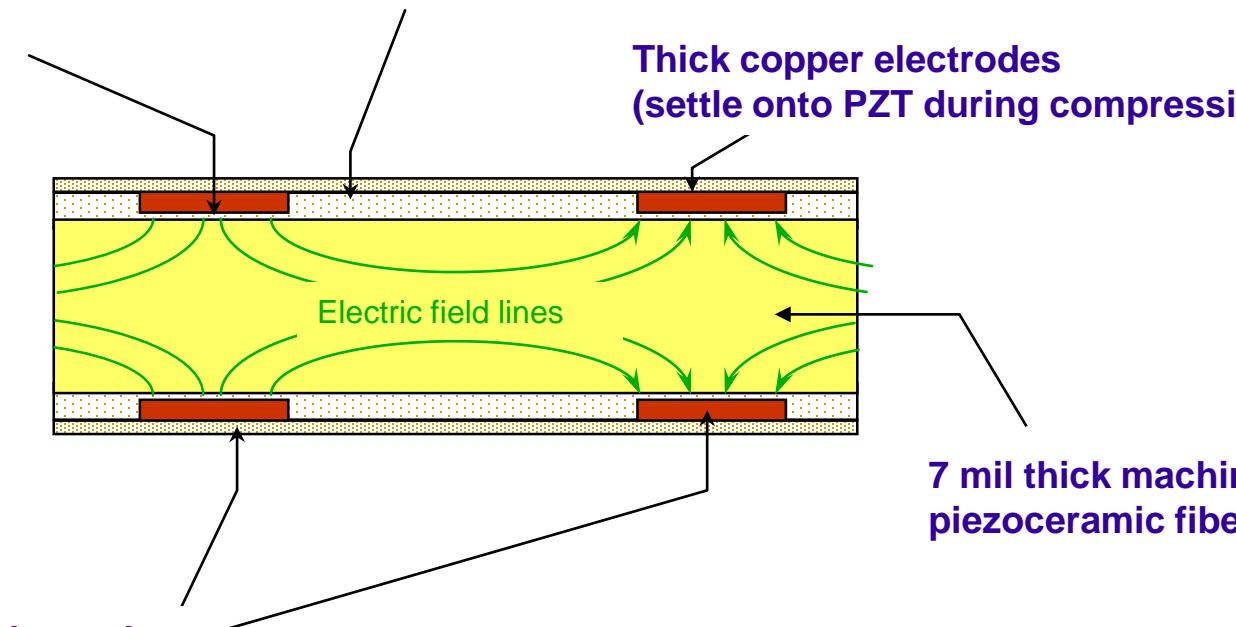
“Starved” bond-line between electrode pad and PZT (only slight electric field attenuation)

Nonconductive thermoset epoxy adhesive (also fills gaps)

Thick copper electrodes (settle onto PZT during compression)

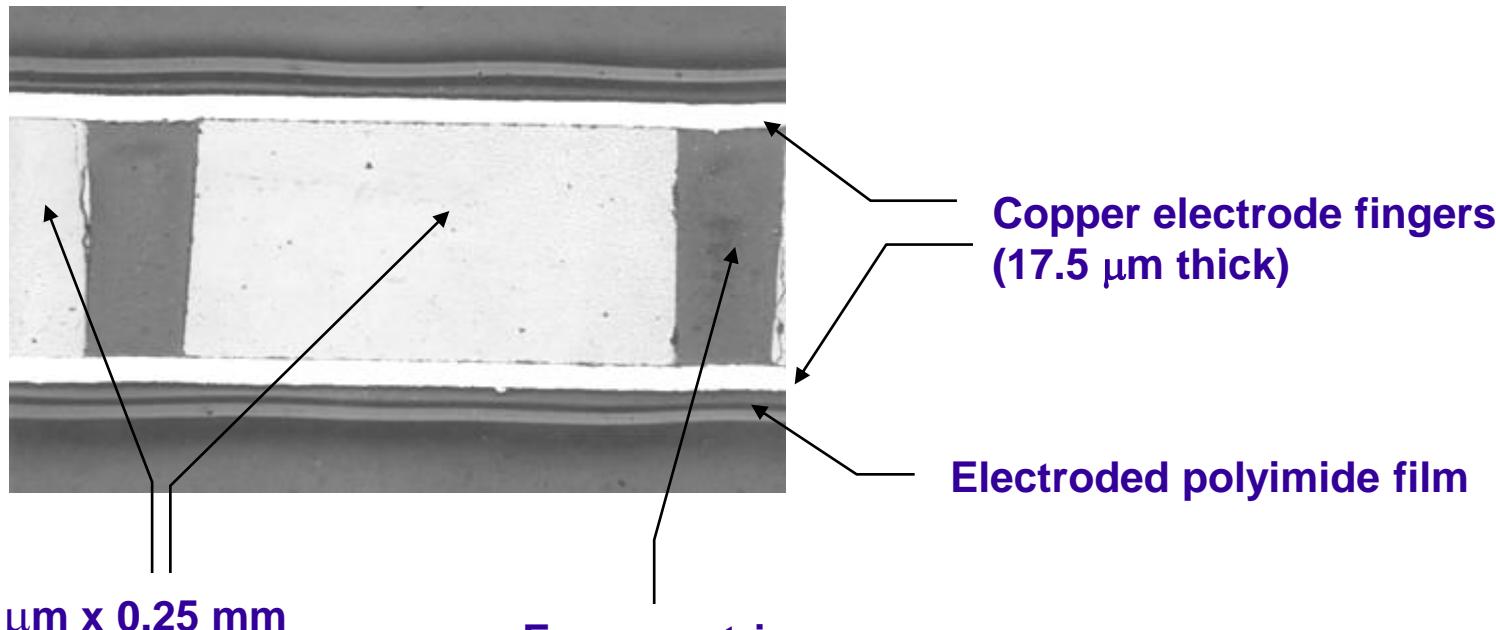
Fiber length axis

Alternately charged electrode fingers on polyimide film (t/b)

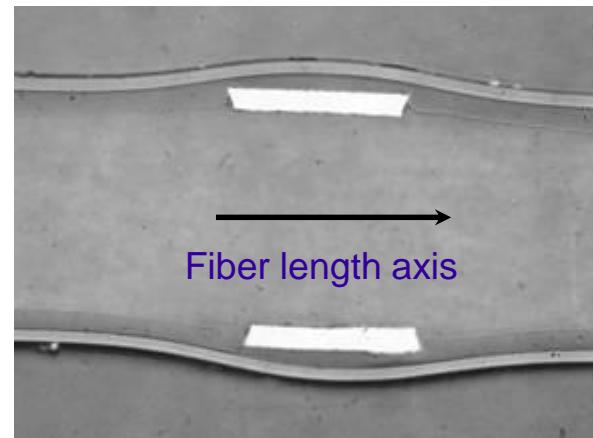


(section along fiber axis)

Epoxy-Only Electrode Attachment ("ZAF-less "MFC")

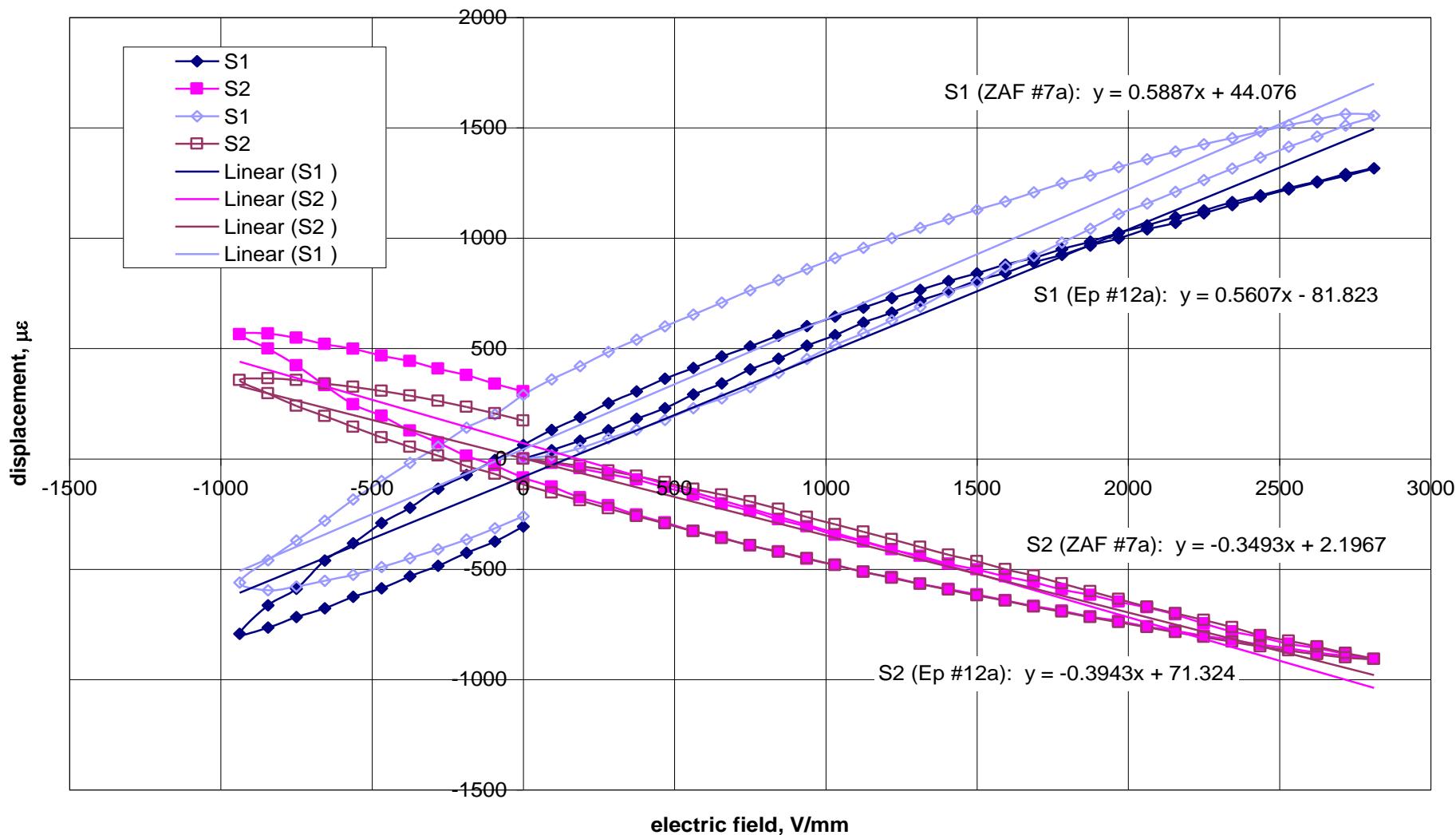


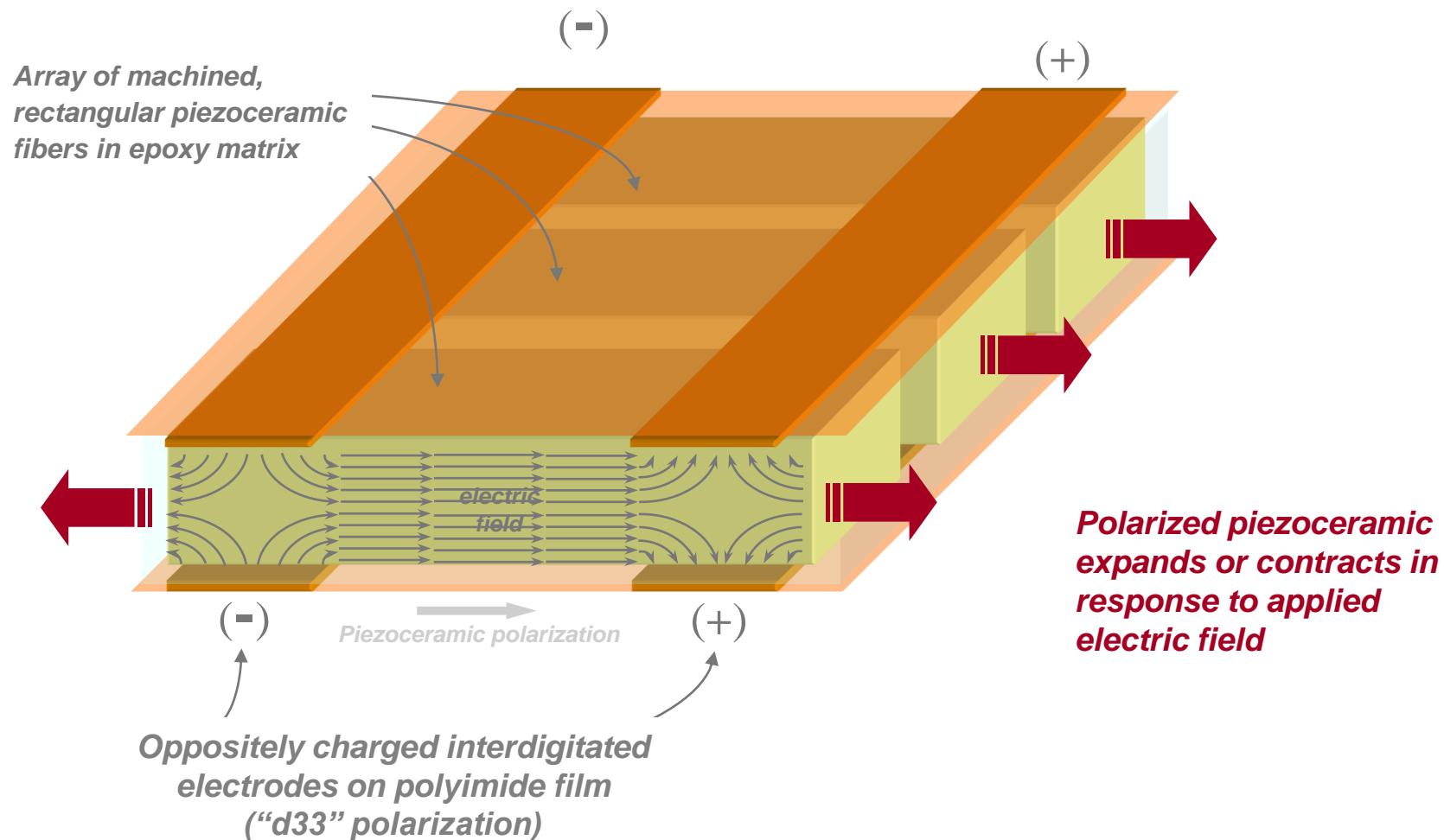
(A-A) Microphotograph across fiber axis.



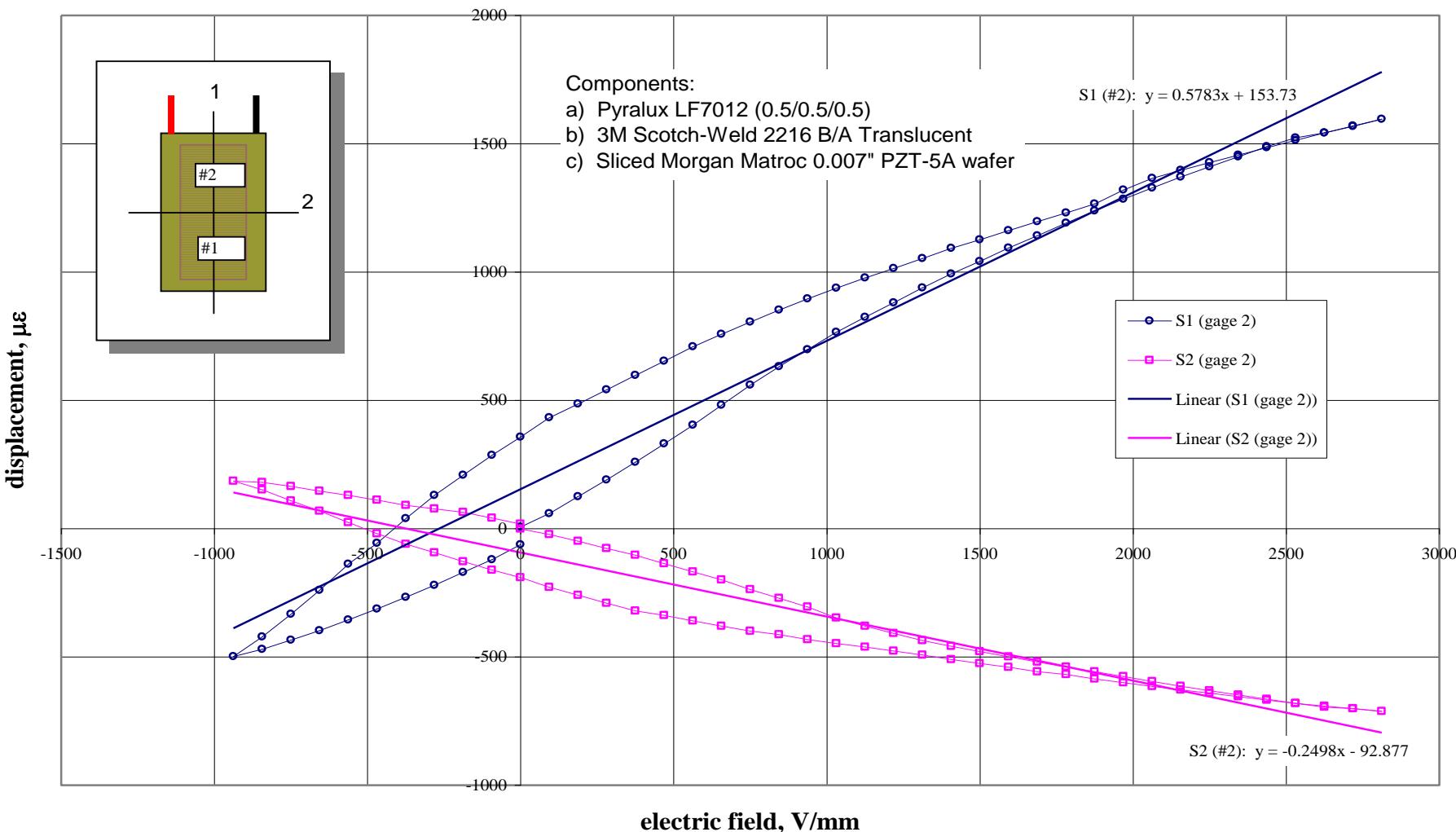
(B-B) Microphotograph along fiber axis.

Reference Actuators: ZAF versus Epoxy Electrode Attachment





Specimen #19: Free-displacement test





MFC Fabrication Process Documentation

JPL

NASA/TM-2003-212427
ARL-TR-2833



Method for Fabricating NASA-Standard Macro-Fiber Composite Piezoelectric Actuators

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Vehicle Technology Directorate
Langley Research Center, Hampton, Virginia

June, 2003

(12) **United States Patent**
Wilkie et al.

(19) **Patent No.:** US 6,629,341 B2
(45) **Date of Patent:** Oct. 7, 2003



US06620341B2

(54) **METHOD OF FABRICATING A PIEZOELECTRIC COMPOSITE APPARATUS**

(75) **Inventors:** W. Keats Wilkie [001], Williamsburg, VA [002]; Robert G. Bryant [001], New York, NY [002]; Robert E. Forti, Hayes, VA [001]; Richard F. Hellmann, Hampton, VA [001]; James W. High, Norfolk, VA [001]; Antonio Jahnke, Jr., Newport News, VA [001]; Bruce D. Ermak, Gloucester, VA [001]; Paul H. Mirkle, Graham, VA [001]

(73) **Assignee:** The United States of America as represented by the Administrator of the National Aeronautics and Space Administration, Washington, DC, (US)

(*) **Notice:** Subject to my disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. §154(b) by 0 days.

(21) **Appl. No.:** 09/424,677

(22) **Filed:** Oct. 28, 1999

(10) **Prior Publication Data**

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(31) **Int. Cl.:** 1004H 17/00

(52) **U.S. CL.:** 29/25.35, 29/34, 29/35, 29/35.1,
29/36.1, 310/326, 310/334, 309/336, 156/222,
156/229, 256/300, 156/301

(50) **Field of Search:** 29/25, 35, 354,
29/35, 689, 1, 832, 837, 840, 310/357,
306, 327, 328, 332, 366, 367, 324, 336,
156/222, 299, 308, 301, 427/6, 180

(56) **References Cited**

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A. A. Best, "Active fiber composite material systems for structural control applications", SPIE Proceedings, Newport Beach, CA, Mar. 1998, pp. 161-171.

A. A. Best et al., "Improved performance in piezoelectric fiber composites using interdigitated electrodes", SPIE vol. 2441, San Diego, CA, Feb. 27-28, 1995, pp. 106-122.

J. P. Rodgers et al., "Characterization of interdigitated electrode piezoelectric fibers and actuators under high electrical and mechanical loading", SPIE vol. 2713, San Diego, CA, Feb. 27-28, 1996, pp. 642-659.

(List continued on next page.)

Primary Examiner—Debra Taggart

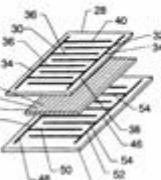
Assistant Examiner—Paul D. Kim

(74) **Attorney, Agent, or Firm:** Kurt G. Hammock

(77) **ABSTRACT**

A method for fabricating a piezoelectric macro-fiber composite actuator comprises providing a piezoelectric material that has two sides and attaching one side upon an adhesive backer sheet. The piezoelectric material is then sliced, the piezoelectric material is then formed into a plurality of piezoelectric fibers in juxtaposition. A conductive film is then adhesively bonded to the other side of the piezoelectric material, and the adhesive backer sheet is removed. The conductive film has first and second conductive patterns formed thereon which are spaced apart, include first and second conductive areas in electrical contact with the piezoelectric material. The first and second conductive patterns of the conductive film each have a plurality of electrodes to form a pattern of interdigitated electrodes. A second film is then bonded to the other side of the piezoelectric material. The second film may have a pair of conductive patterns similar to the conductive patterns of the first film.

15 Claims, 6 Drawing Sheets



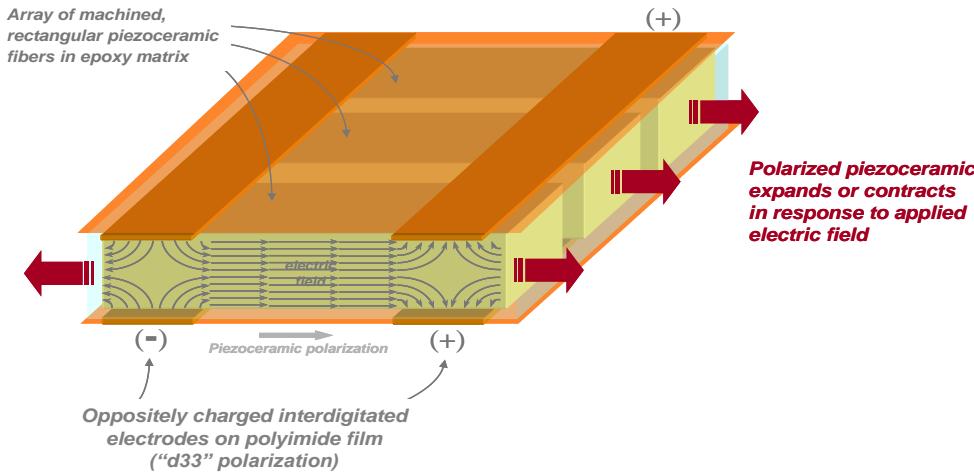


LaRC-MFC: 2000 R&D100 Award Winners

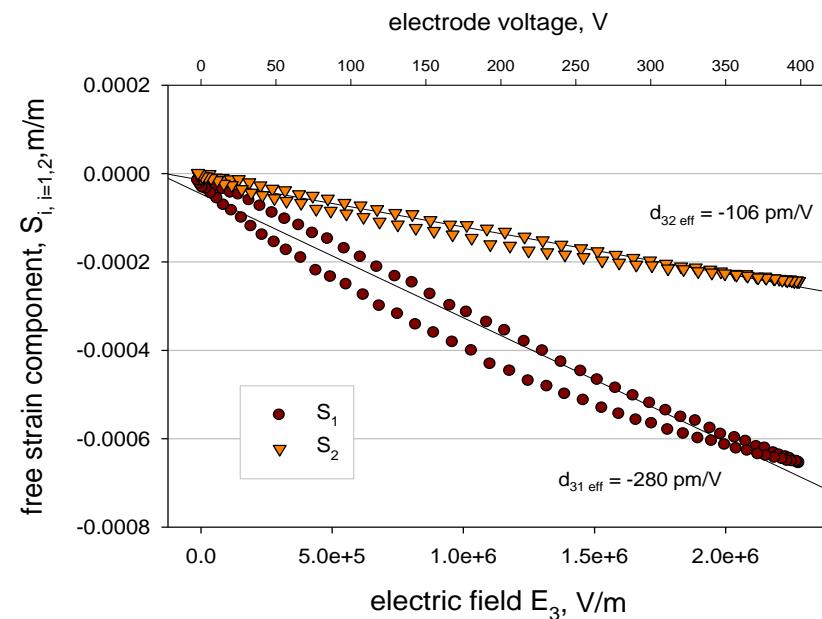
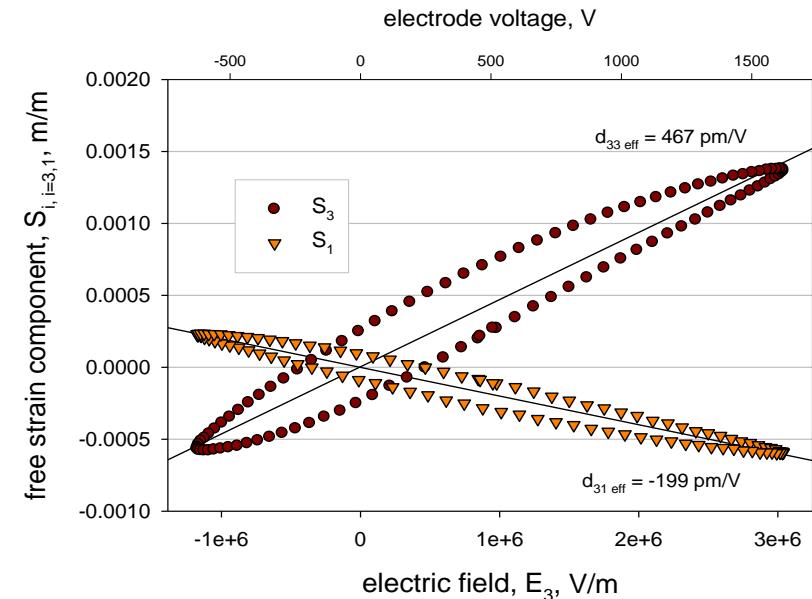
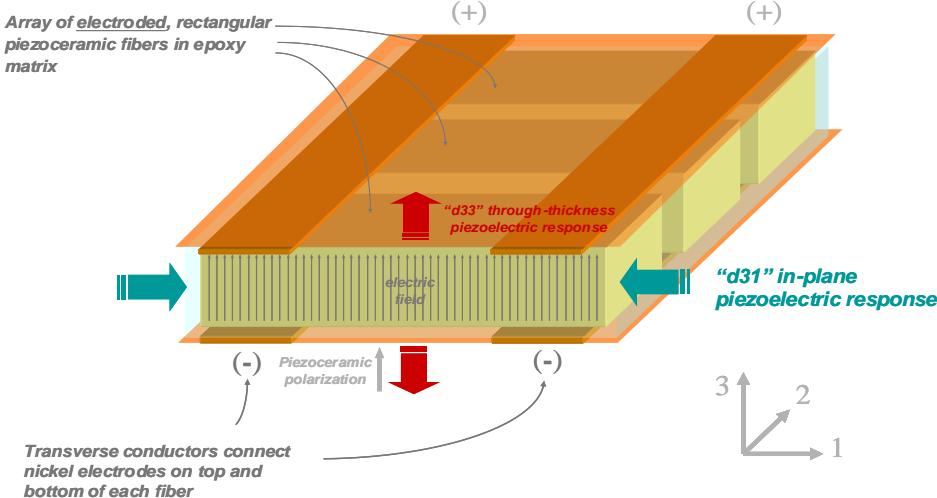
JPL

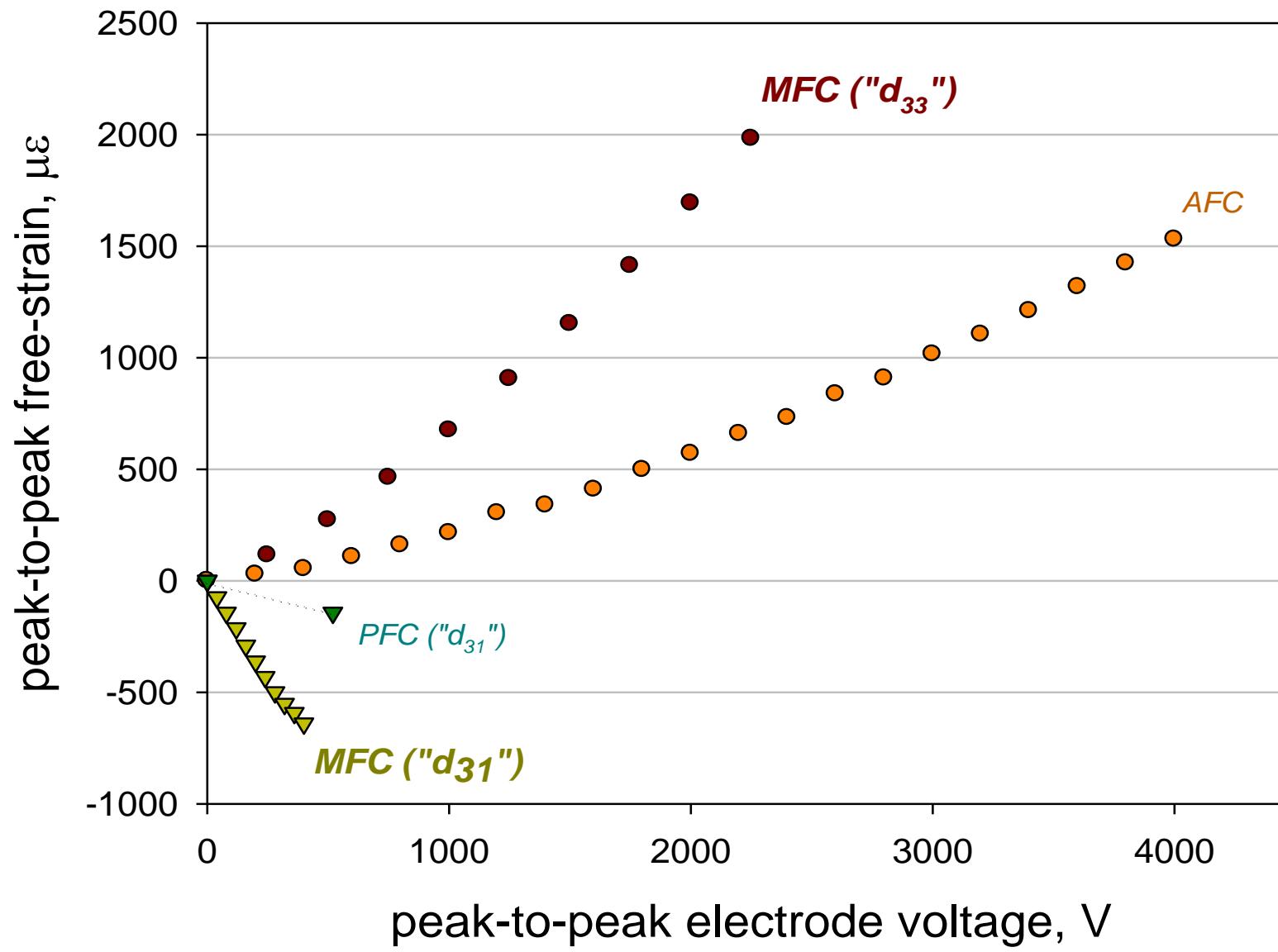


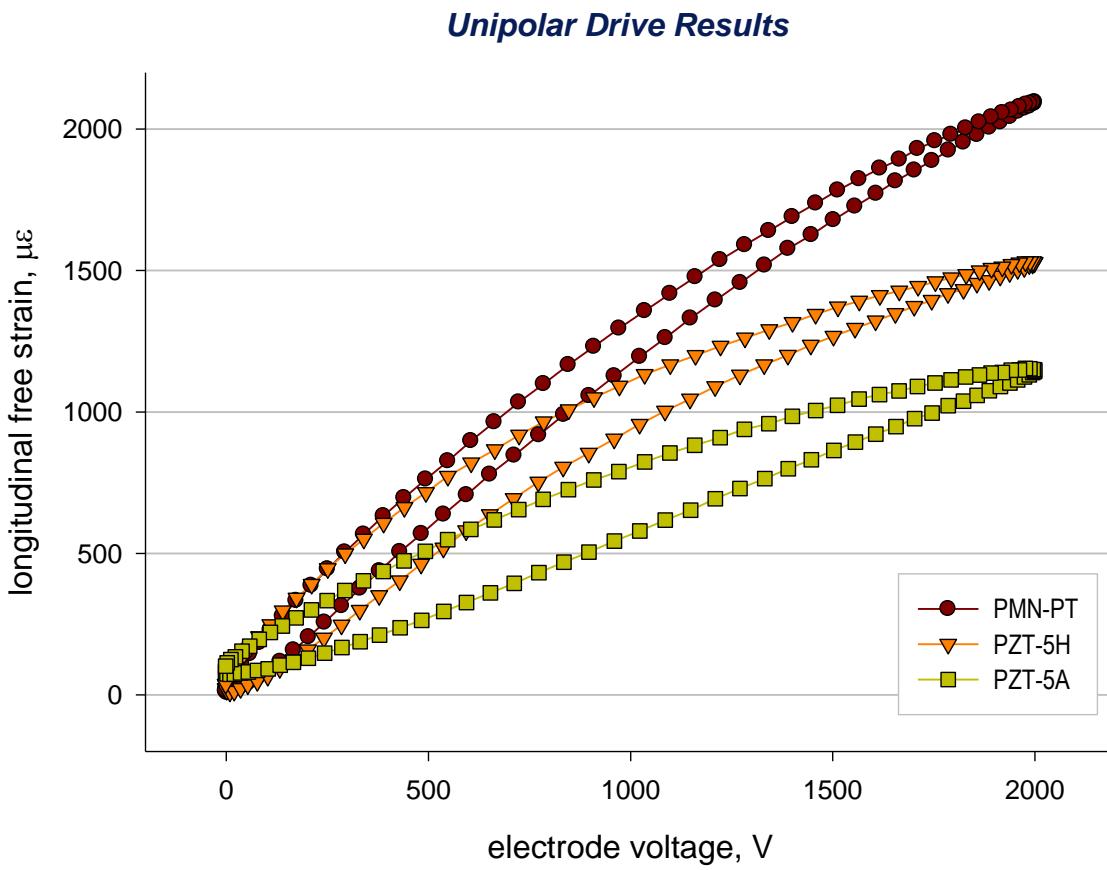
Standard “ d_{33} ” polarization



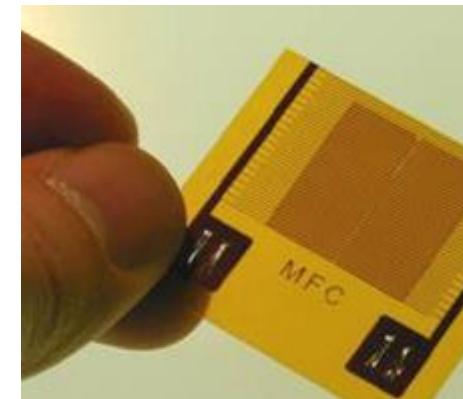
Alternate “ d_{31} ” polarization







20 mm MFC Test Specimens



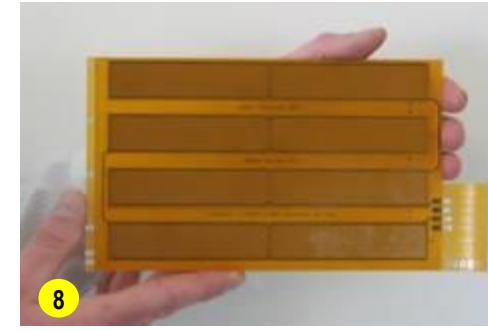
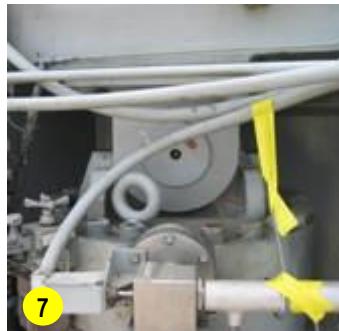
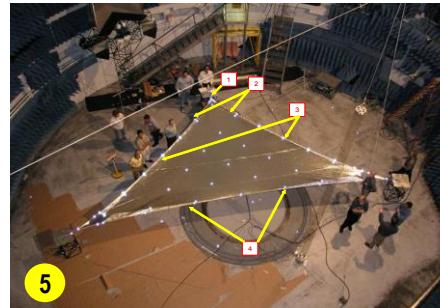
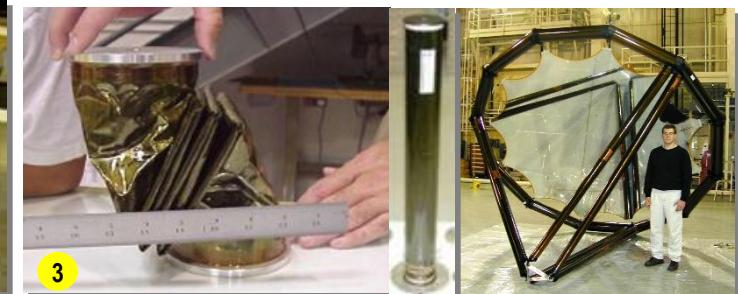
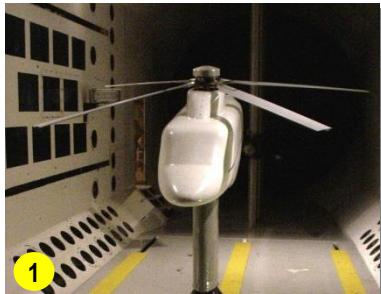
material	$S_3/S_{3,PZT-5A}^{\dagger}$	$\bar{d}_{33}/\bar{d}_{33,PZT-5A}$	$\Delta\%_{3-dr}^{\ddagger}$
PZT-5A	1.0	1.0	-
PZT-5H	1.40	1.66	+18.6%
PMN-PT	1.96	4.88	+149%

$$\bar{d}_{33} = \frac{d_{33,f}}{\left(1 + \frac{\phi_m}{\phi_f} \frac{s_{33,f}^E}{s_{33,m}^E}\right)}$$

material	$K_3^T (1kHz)$	k_{33}	$d_{33}, pm/V$	$d_{31}, pm/V$	$\rho, g/cm^3$	$S_{33}^E \dagger$	S_{11}^E	S_{13}^E	S_{44}^E
PZT-5A	1900	0.72	390	-190	7.8	18.8	16.4	-7.22	47.5
PZT-5H	3800	0.75	650	-320	7.8	20.7	16.5	-9.1	43.5
PMN-PT	7151	0.91	2285	-1063	8.05	86.5	59.7	-45.3	14.4

[†]elastic constants, s, $10^{-12} m^2/N$

Refs.: Jaffe, Cook, Jaffe; CTS Wireless; Morgan-Matroc, TRS



- ① Active Twist Rotor (NASA, ARL, University of Michigan, Sikorsky), ② Twin-tail buffet loads alleviation (NASA, AFRL, Boeing), ③ Active inflatable-rigidizable spacecraft structures (NASA, JPL, DoD, L'GARDE, ILC Dover), ④ On-orbit rigidizable structures dynamics Shuttle flight experiment (AFIT), ⑤ Solar-sail structures on-orbit dynamics system identification (NASA, AEC Able), ⑥ KSC launch tower white room impedance-based health monitoring (Virginia Tech, LANL), ⑦ KSC crawler bearing health monitoring (Virginia Tech, LANL), ⑧ Automotive drive shaft active vibration damping (Volkswagen R&D, Smart Material Corp.), and ⑨ Structural loads sensing and energy harvesting (University of Munich, Storck Bicycle, Smart Material Corp.)



Special Thanks

JPL

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Virginia Tech, CIMSS

Brett Williams

NASA JPL

Richard Cobb

USAF, AFIT, Dayton, OH

Jim Gaspar

NASA Langley Research Center, Structural Dynamics Branch

Marc Schultz

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Billy Derbes

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Kurt Hammerle

NASA Johnson Spaceflight Center

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Jim Linker

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Kathy Kuykendal

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